



Principle of EE1

Lesson 4

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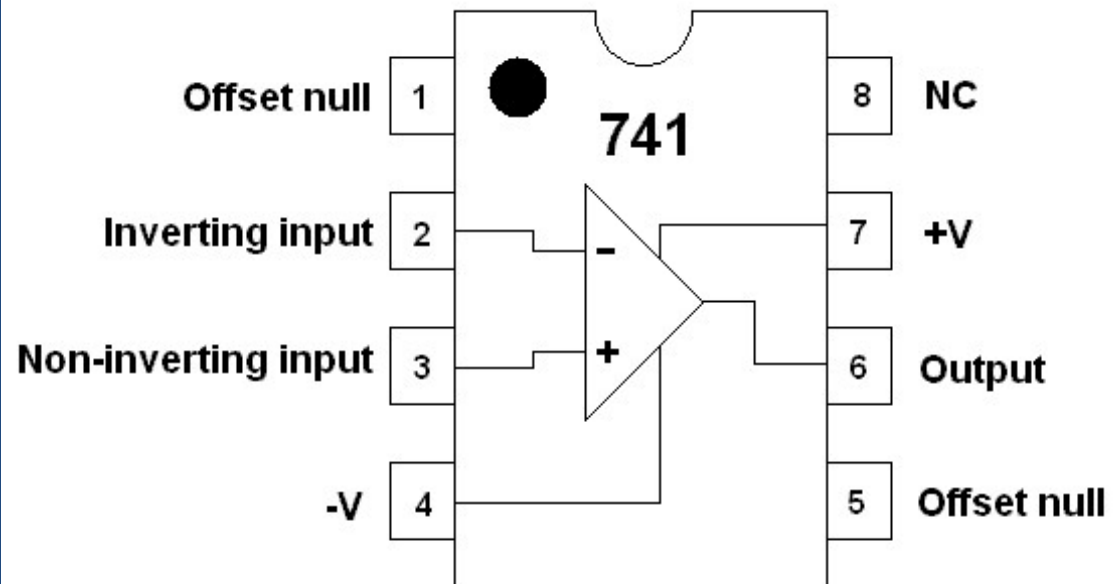
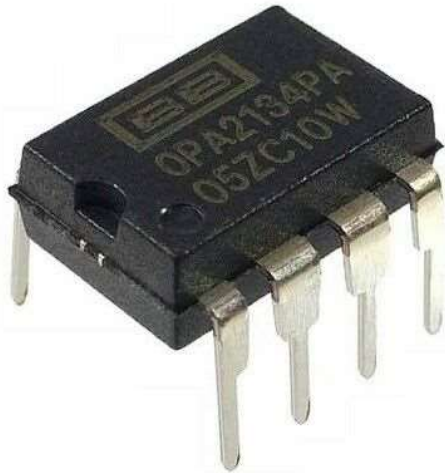
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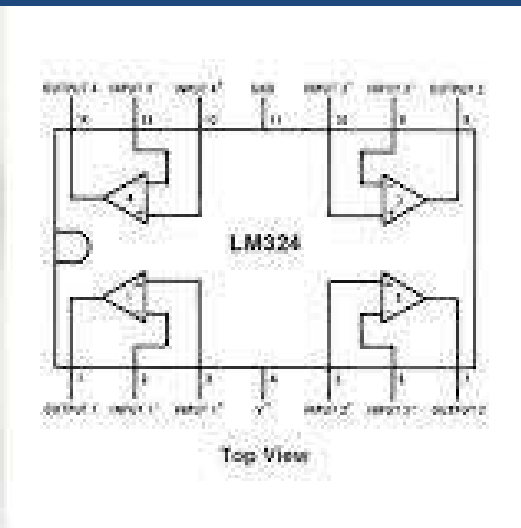
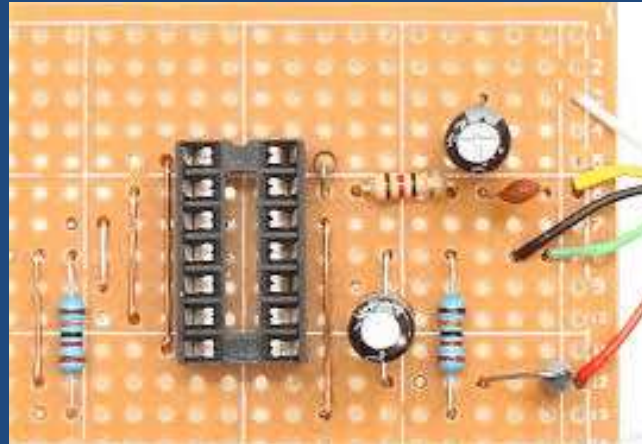
OPERATIONAL AMPLIFIER (OP-AMP)

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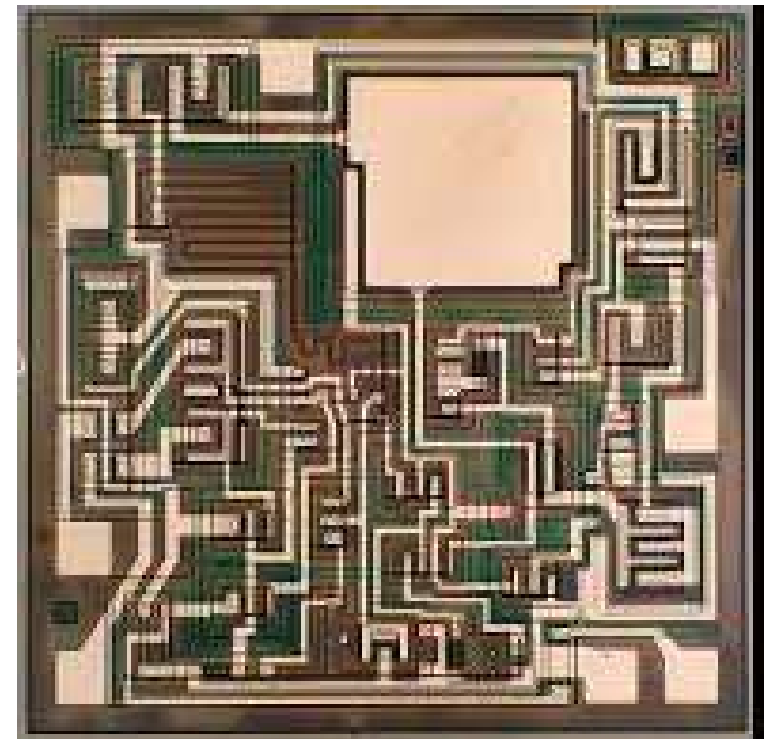
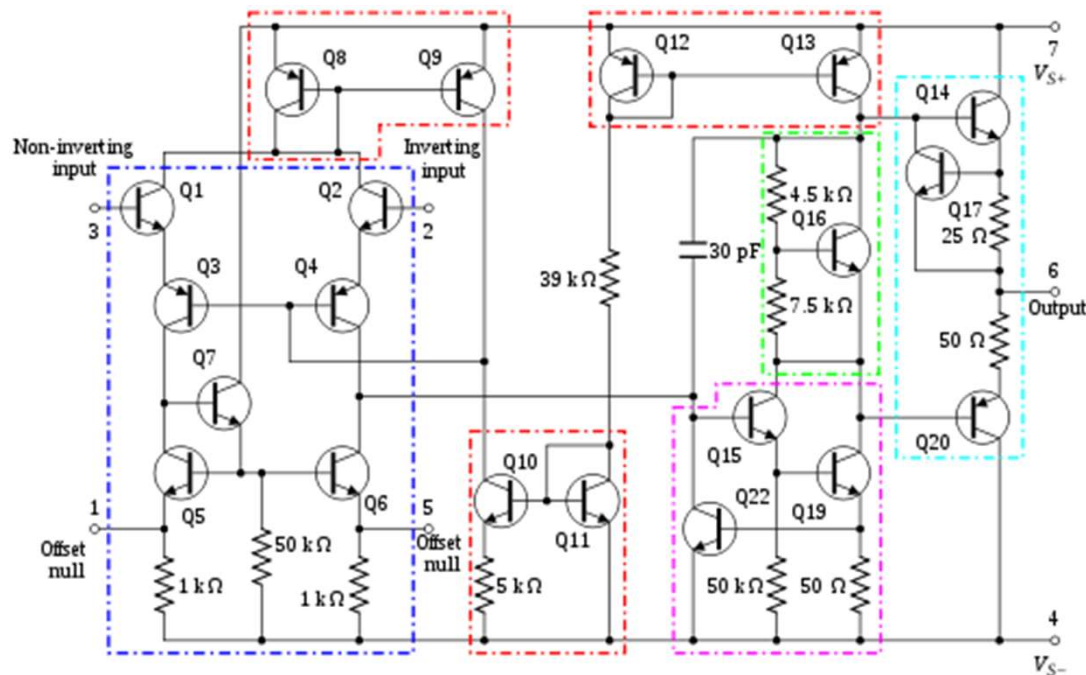
- Physical aspect of an op-amp
- Op-amp characteristics
- Negative feedback circuit:
 - Applications of op-amp
 - Analysis of an op-amp circuit
 - Different features of op-amp utilization
- Real world op-amp

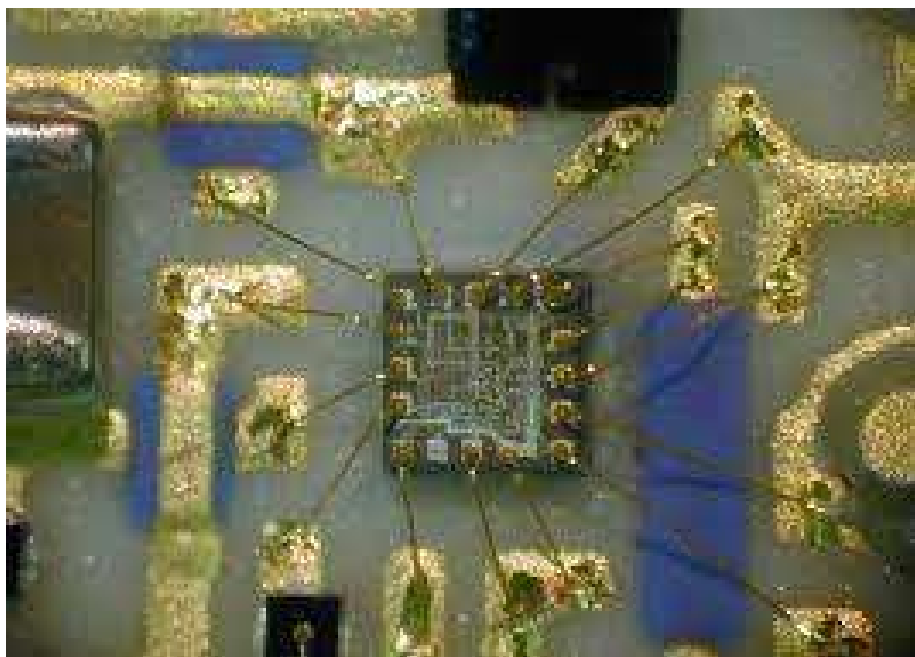
OPERATIONAL AMPLIFIER (Op-Amp)



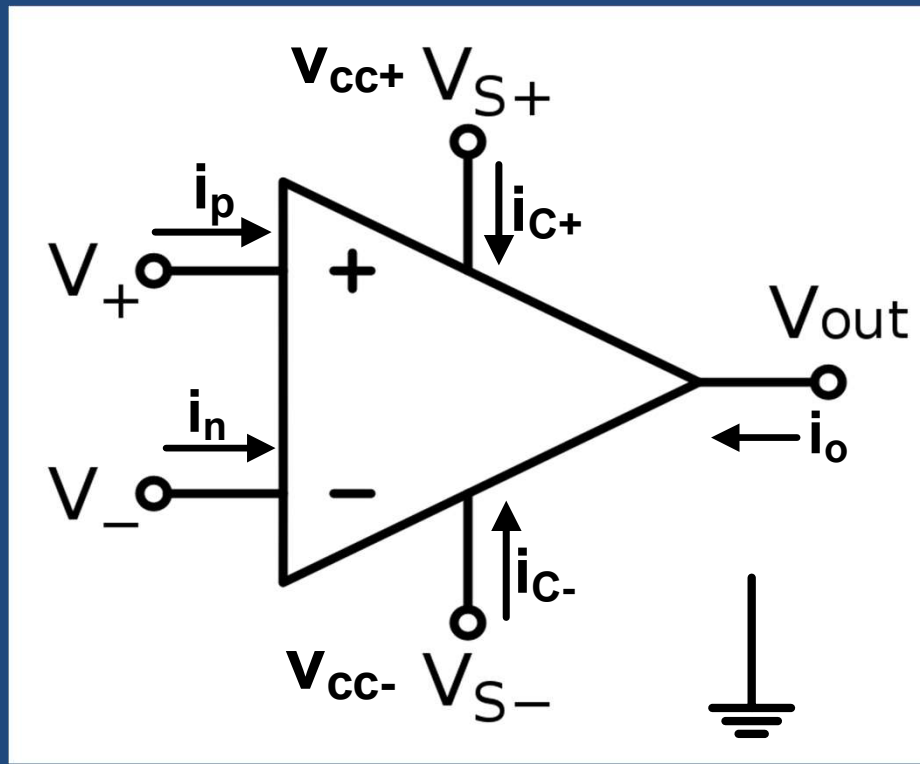


Very large-scale integration (VLSI) Technology

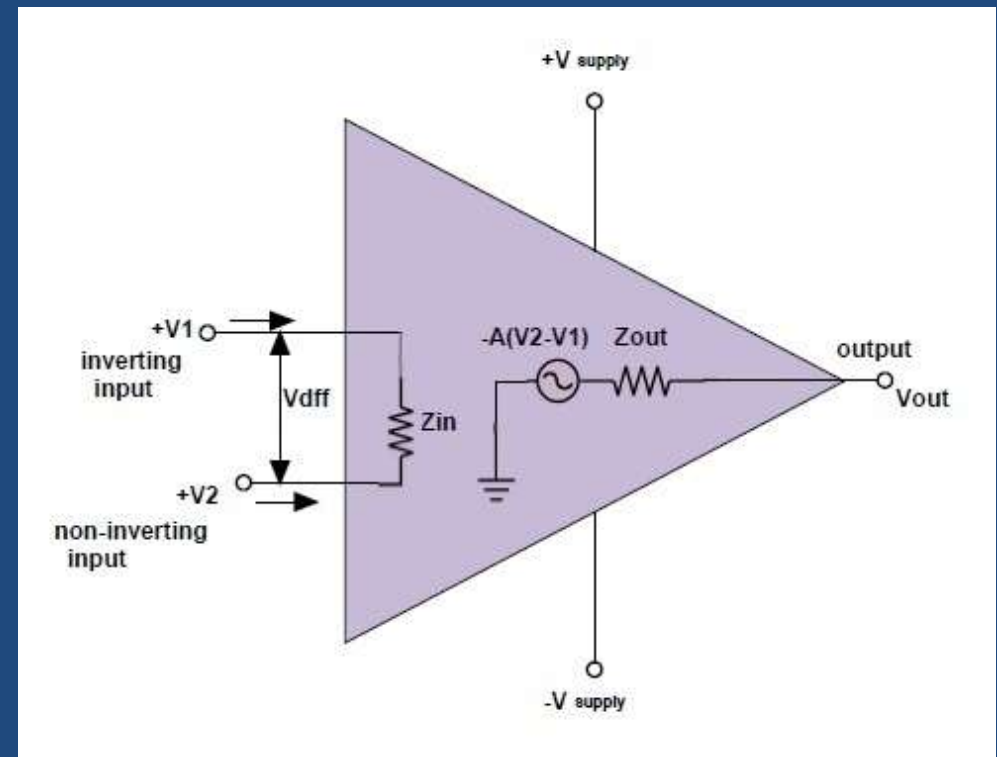




Op-Amp Basics



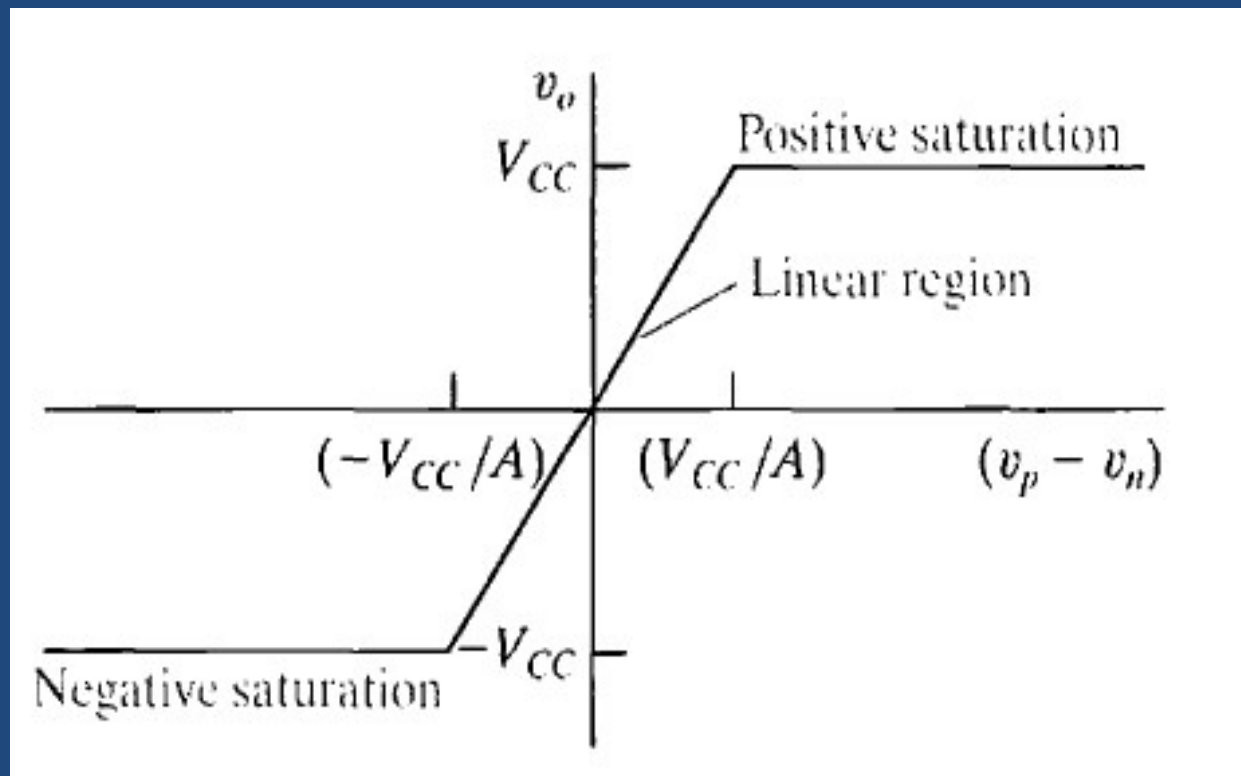
Ideal op-amp



Real op-amp

Characteristics of an ideal op-amp

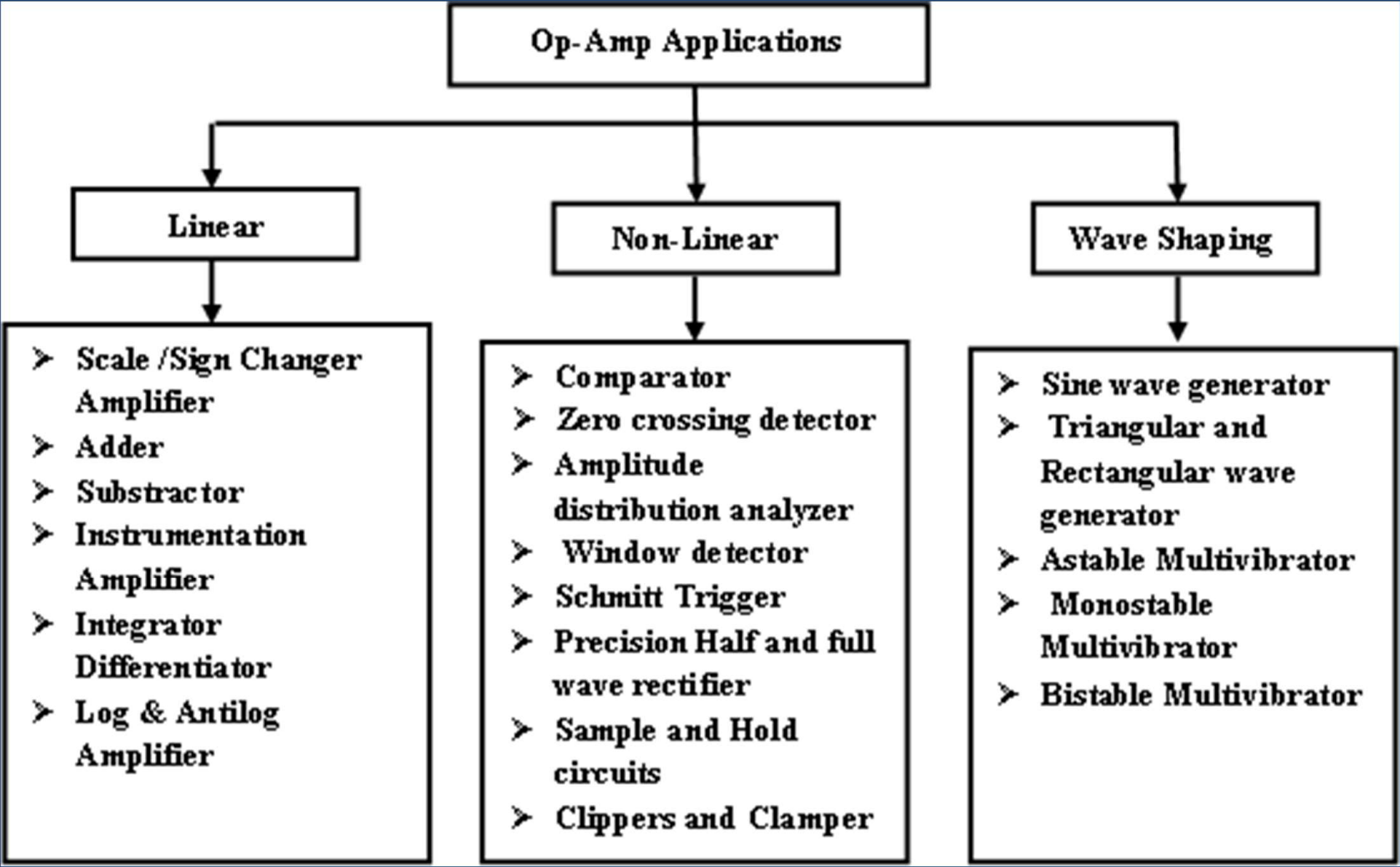
1. Linear vs. saturated zones



Characteristics of an ideal op-amp

1. Linear vs. saturated zones
2. Infinite input impedance $\Rightarrow I_p = I_n = 0$
3. Zero output impedance
4. Infinite voltage gain
5. Zero common mode gain
6. Infinite bandwidth

Op-Amp Applications



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graph TD; A[Op-Amp Applications] --> B[Linear]; A --> C[Non-Linear]; A --> D[Wave Shaping]; B --> E["> Scale /Sign Changer Amplifier<br/>> Adder<br/>> Subtractor<br/>> Instrumentation Amplifier<br/>> Integrator<br/>> Differentiator<br/>> Log & Antilog Amplifier"]; C --> F["> Comparator<br/>> Zero crossing detector<br/>> Amplitude distribution analyzer<br/>> Window detector<br/>> Schmitt Trigger<br/>> Precision Half and full wave rectifier<br/>> Sample and Hold circuits<br/>> Clippers and Clamper"]; D --> G["> Sine wave generator<br/>> Triangular and Rectangular wave generator<br/>> Astable Multivibrator<br/>> Monostable Multivibrator<br/>> Bistable Multivibrator"];
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Linear

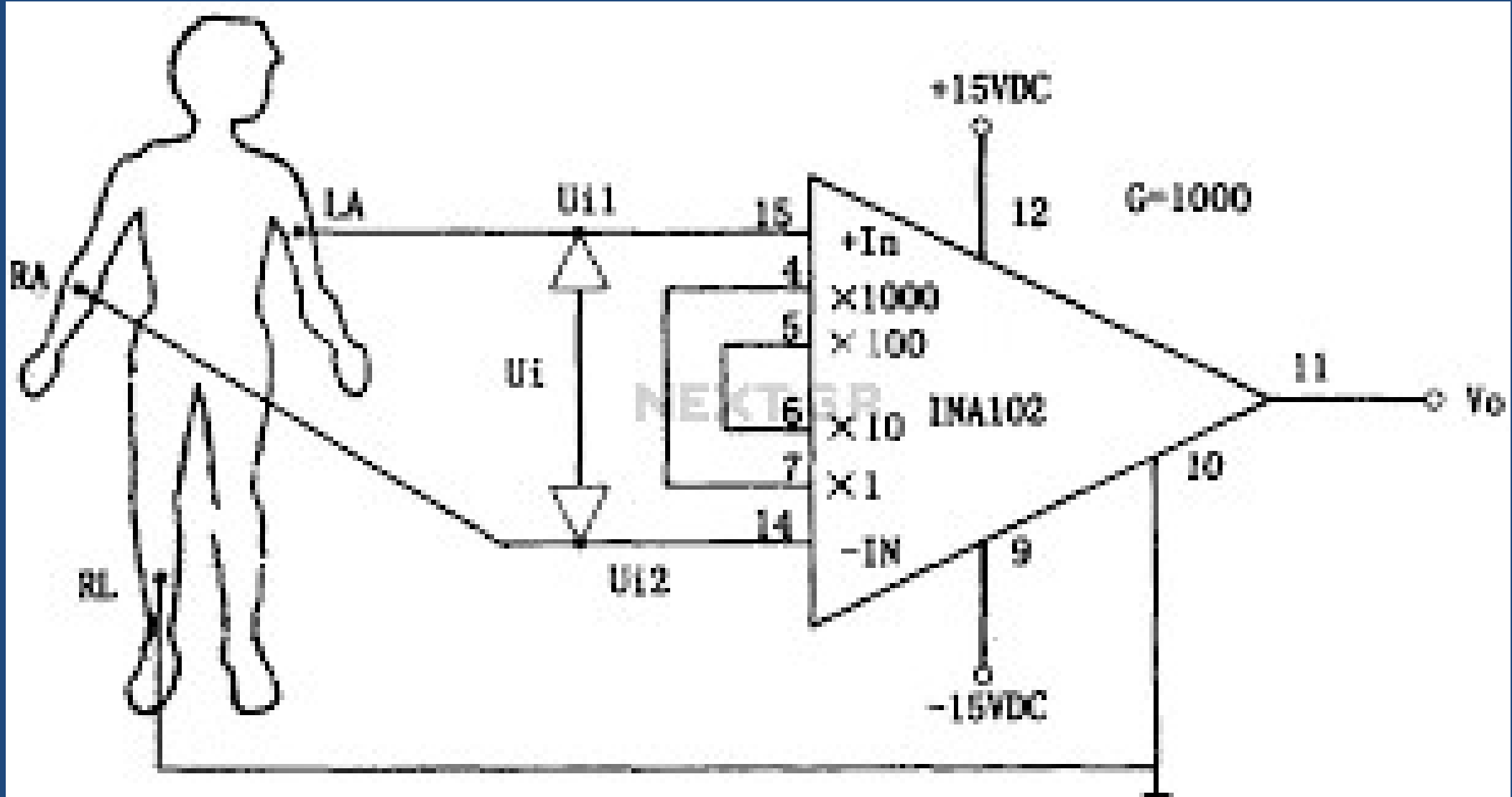
- Scale /Sign Changer Amplifier
- Adder
- Subtractor
- Instrumentation Amplifier
- Integrator
- Differentiator
- Log & Antilog Amplifier

Non-Linear

- Comparator
- Zero crossing detector
- Amplitude distribution analyzer
- Window detector
- Schmitt Trigger
- Precision Half and full wave rectifier
- Sample and Hold circuits
- Clippers and Clamper

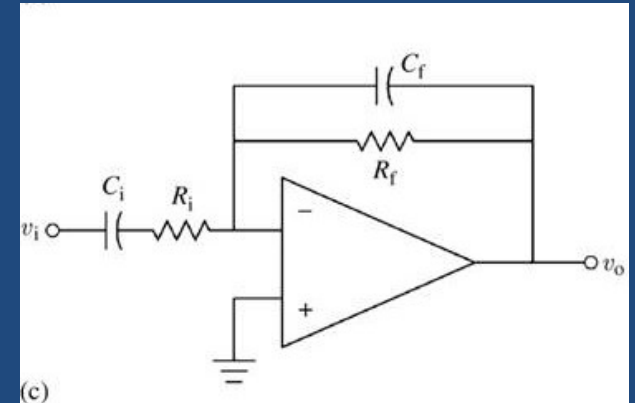
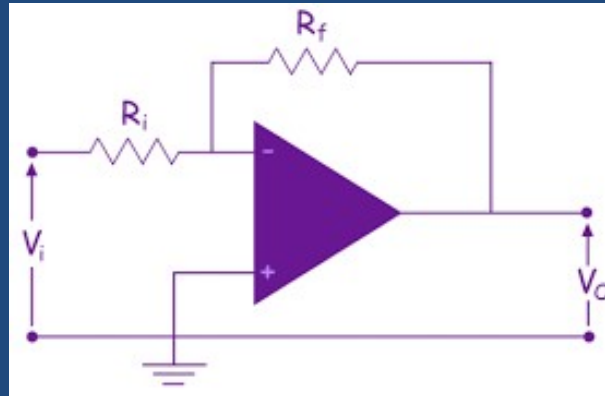
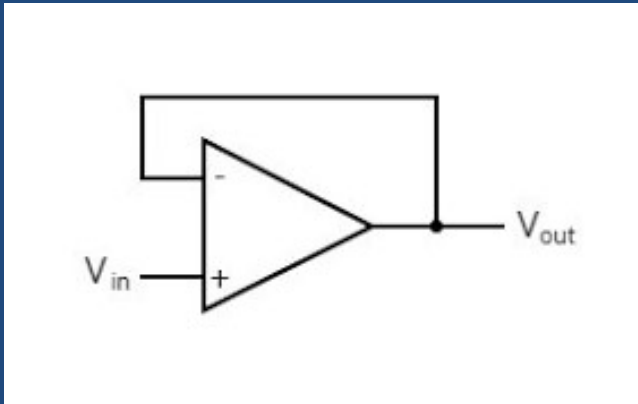
Wave Shaping

- Sine wave generator
- Triangular and Rectangular wave generator
- Astable Multivibrator
- Monostable Multivibrator
- Bistable Multivibrator



Negative Feedback

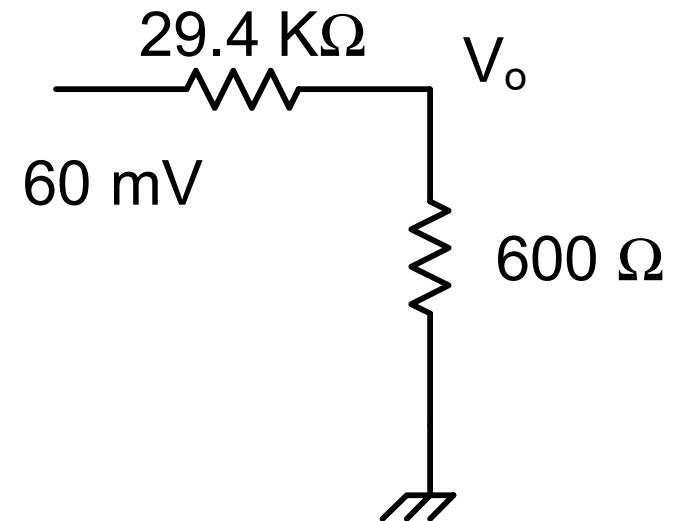
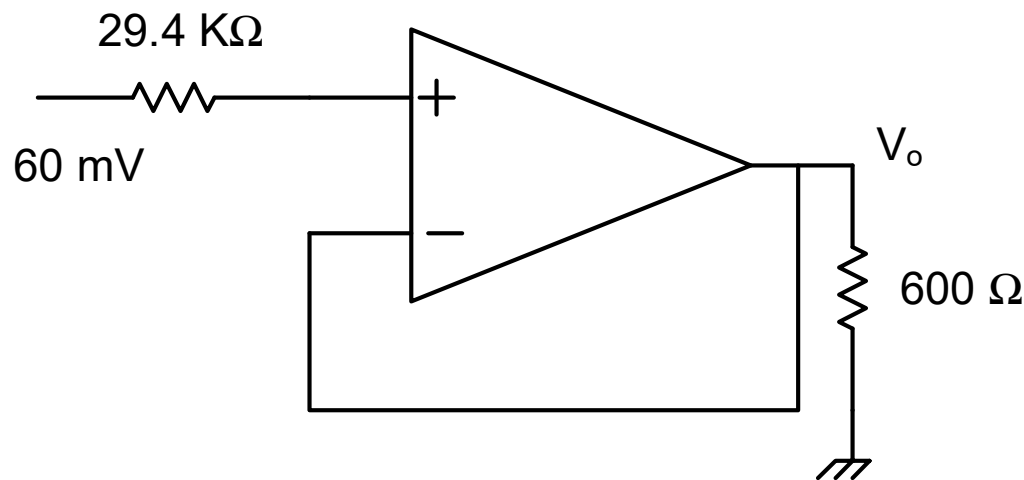
1. $v_p = v_n$
2. $i_p = i_n = 0$



ANALYSIS OF A CIRCUIT USING OP-AMP

Role of an Op-Amp

What are the gains in voltage and power at 600Ω in both situations?



Role of an Op-Amp (cont.)

* With op-amp:

$$i_p = i_n = 0$$

$$v_p = v_n = 60 \times 10^{-3} \text{ V}$$

$$v_o = v_{in} = 60 \times 10^{-3} \text{ (voltage follower)}$$

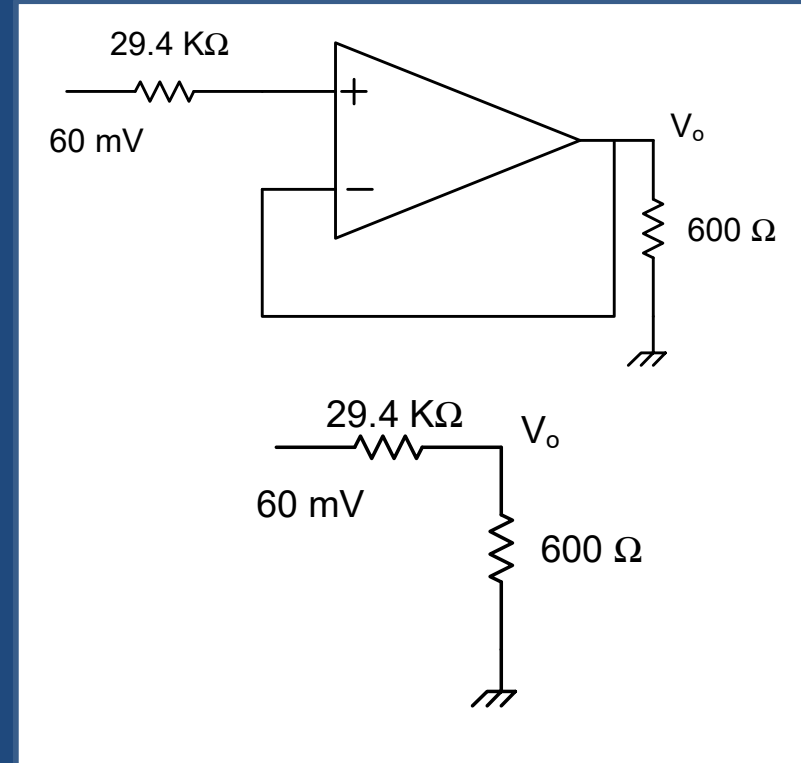
$$P = (0.06)^2 / 600 = 6 \times 10^{-6} \text{ W}$$

* Without op-amp:

$$v_o = 60 \times 10^{-3} \frac{600}{29,400 + 600} = 1.2 \times 10^{-3} \text{ V}$$

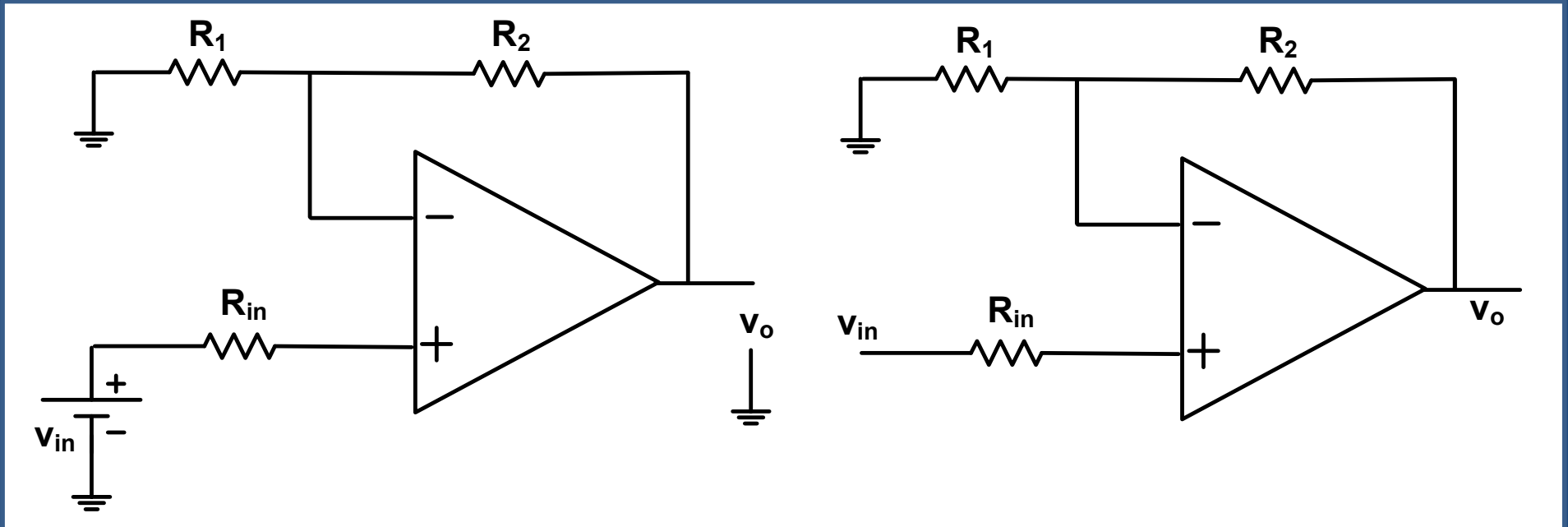
$$P = (1.2 \times 10^{-3})^2 / 600 = 2.4 \times 10^{-9} \text{ W}$$

With op-amp: Voltage gain 50X and
Power gain 2.500X



Non-Inverting input

Given v_{in} and all resistances. Find relationship between v_o and v_{in}



Non-Inverting input (cont.)

1. $i_p = i_n = 0$

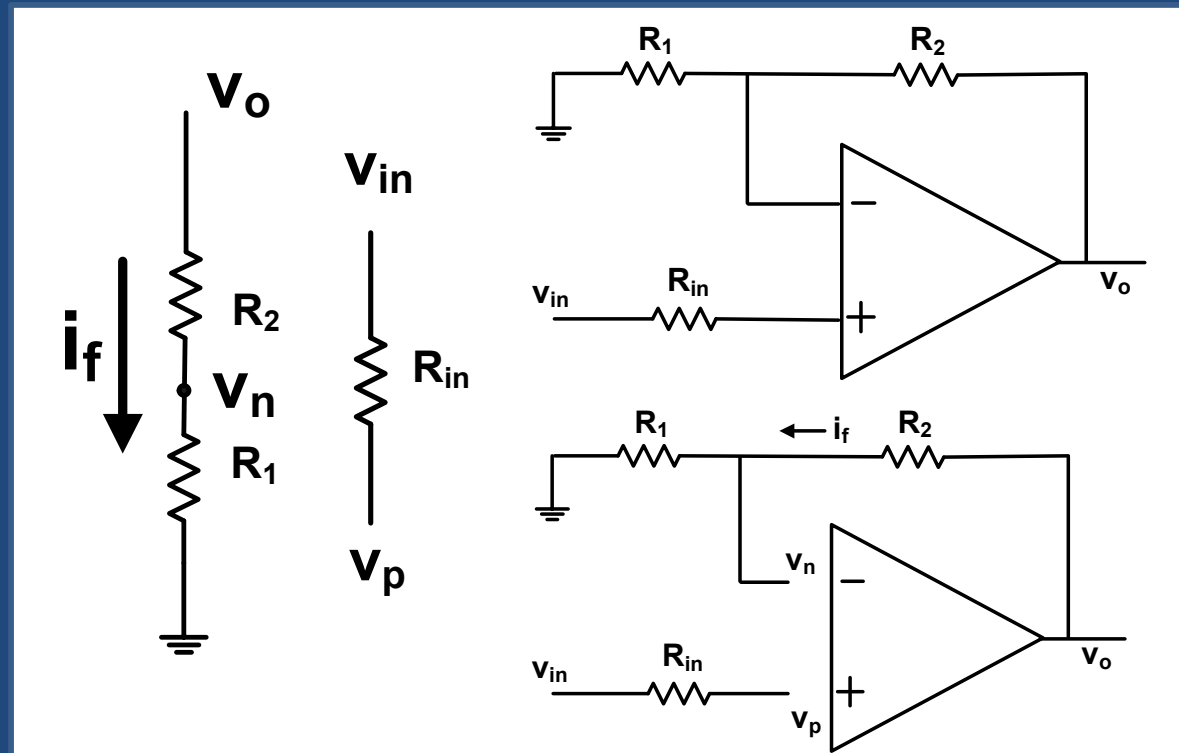
2. $v_p = v_n$

$V_p = V_{in}$

Using voltage divider

$$V_n = V_o \frac{R_1}{R_1 + R_2} = V_{in}$$

$$\Rightarrow V_o = V_{in} \frac{R_1 + R_2}{R_1}$$



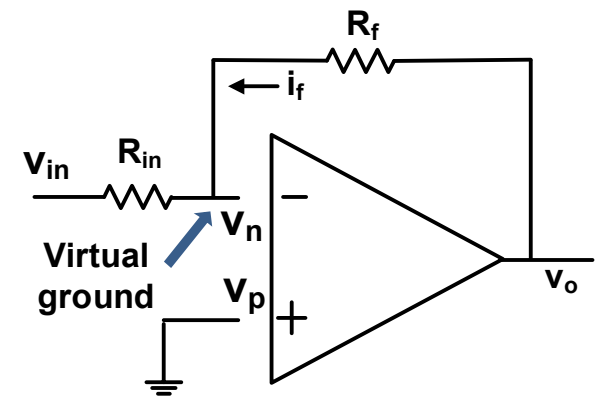
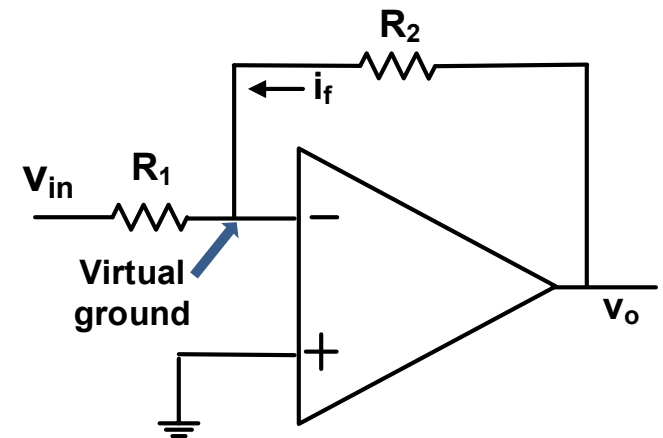
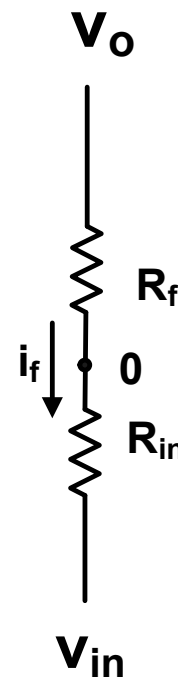
Inverting input

$$1. \quad i_p = i_n = 0$$

$$2. \quad v_p = v_n = 0$$

$$i_f = \frac{v_o}{R_f} = \frac{0 - v_{in}}{R_{in}}$$

$$\Rightarrow v_o = -v_{in} \frac{R_f}{R_{in}}$$



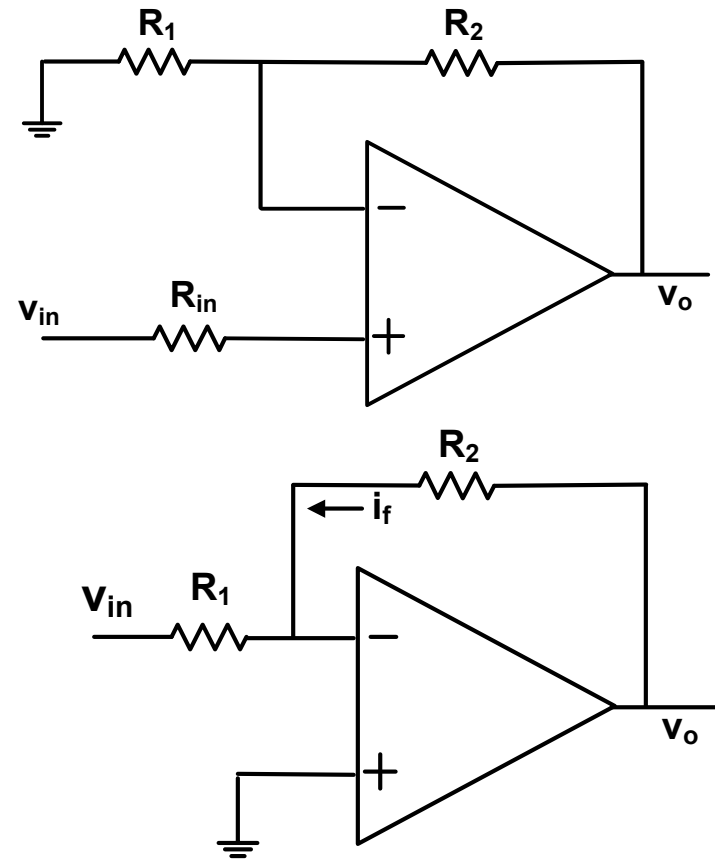
Comparison between Non-Inverting and Inverting input features

$$V_o = V_{in} \frac{R_1 + R_2}{R_1}$$

$v_o \geq v_{in}$ and same sign

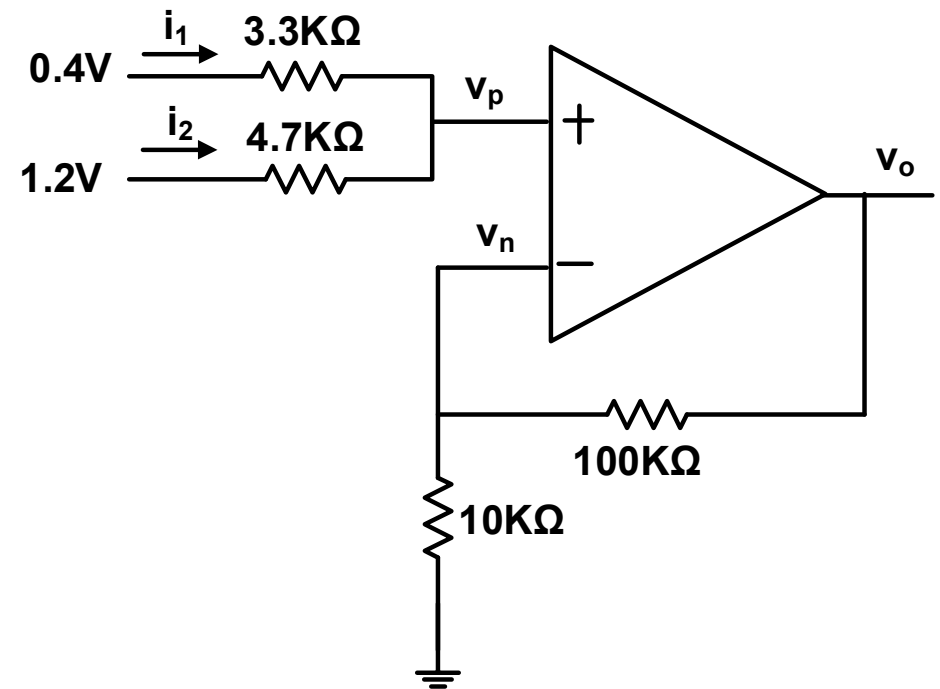
$$V_o = -V_{in} \frac{R_2}{R_1}$$

$v_o \geq v_{in}$ or $v_o \leq v_{in}$ and in opposite sign



Adding 2 non-inverting inputs

Determine v_p and v_o



Solution

$$1. \quad i_p = i_n = 0$$

$$2. \quad v_p = v_n$$

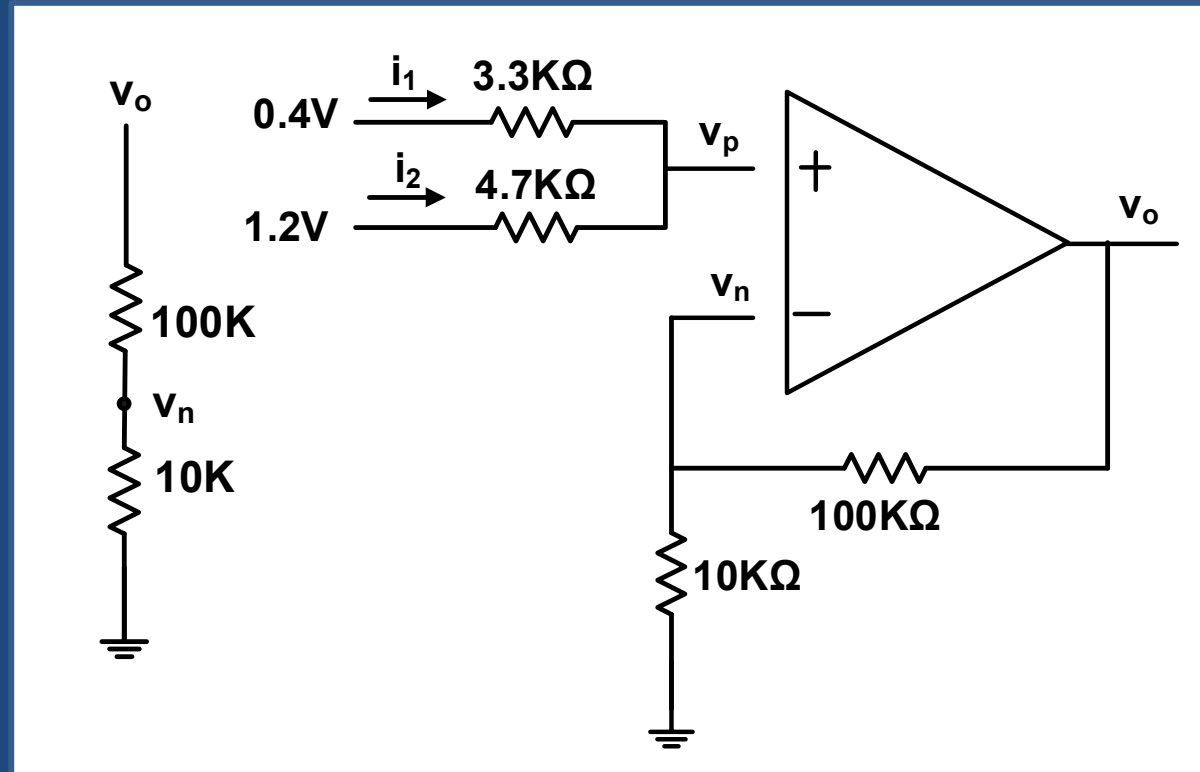
$$i_1 + i_2 = 0$$

$$\frac{0.4 - v_p}{3.3K} + \frac{1.2 - v_p}{4.7K} = 0$$

$$\Rightarrow v_p = \underline{\mathbf{0.73V}}$$

$$v_n = v_o \frac{10K}{10K + 100K} = v_p$$

$$\Rightarrow v_o = 11 v_p = \underline{\mathbf{8.03V}}$$



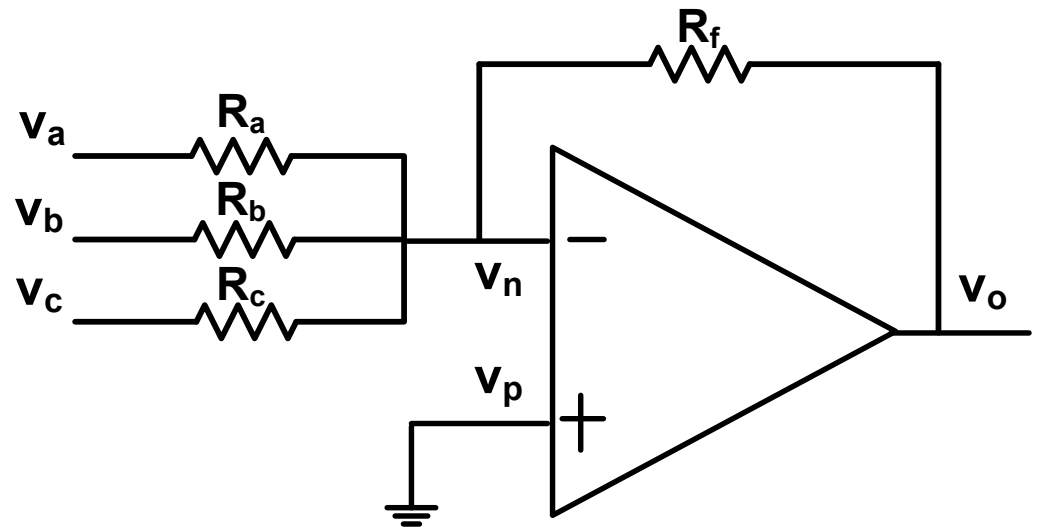
Adding 3 inverting inputs: Summer

1. $i_p = i_n = 0$

2. $v_p = v_n = 0$

$$\frac{V_a}{R_a} + \frac{V_b}{R_b} + \frac{V_c}{R_c} = -\frac{V_o}{R_f}$$

$$\Rightarrow V_o = -R_f \left(\frac{V_a}{R_a} + \frac{V_b}{R_b} + \frac{V_c}{R_c} \right)$$



Current to Voltage Converter

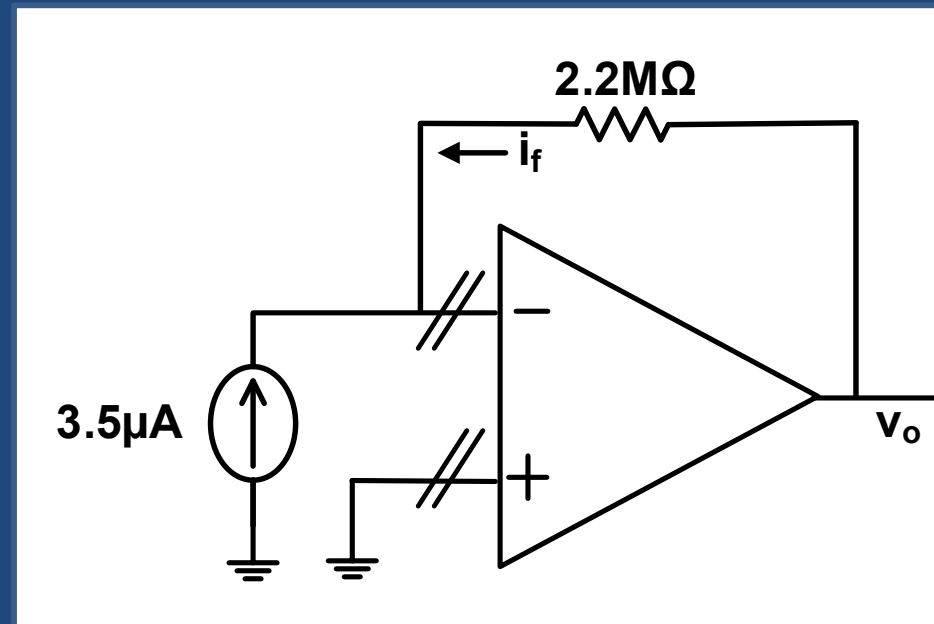
The goal of this circuit is to convert a current source into a voltage source

1. $i_p = i_n = 0$

2. $v_p = v_n = 0$

$i_f = -3.5 \mu\text{A}$

$\Rightarrow v_o = 2.2 \cdot 10^6 (-3.5 \times 10^{-6}) = -7.7 \text{ V}$



Example

Find the range of α so that the op-amp is not saturated

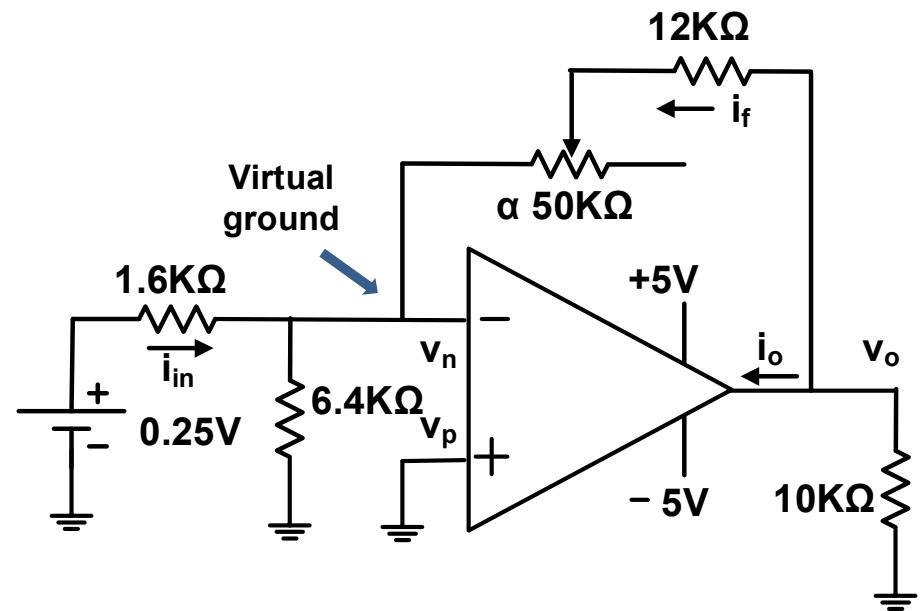
$$\Rightarrow V_o \leq +5V$$

$$\text{Or } V_o \geq -5V$$

$$\text{And } 0 \leq \alpha \leq 1$$

Statement:

1. $i_p = i_n = 0$
2. $v_p = v_n = 0$



Solution

$$i_{in} = \frac{0.25}{1.6K} = -i_f$$

$$v_o = i_f (\alpha 50K + 12K)$$

$$v_o = -\frac{0.25}{1.6K}(\alpha 50K + 12K)$$

$$= -0.16(\alpha 50 + 12)$$

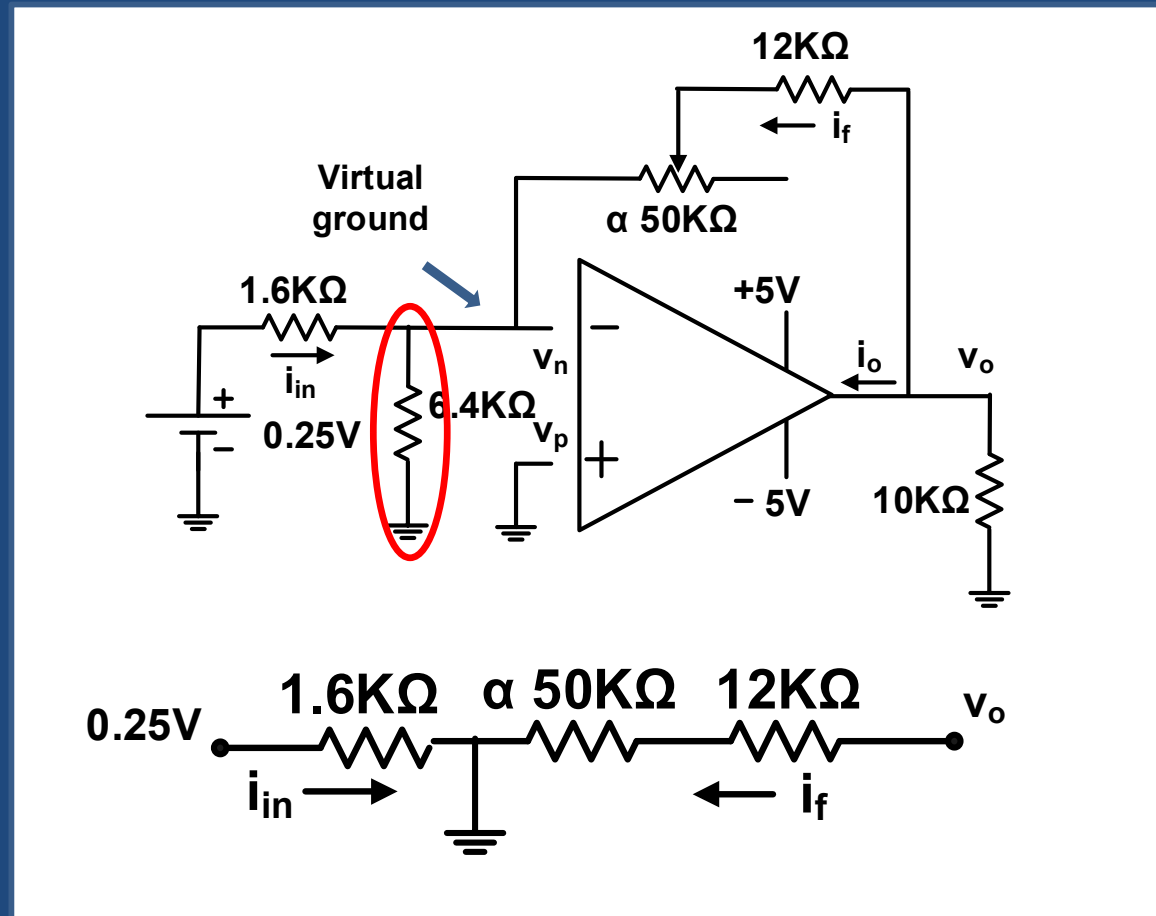
$$* \underline{v_o \geq -5V}$$

$$\Rightarrow \alpha \leq 0.4$$

$$* \underline{v_o \leq +5V}$$

$$\Rightarrow \alpha \geq -0.88$$

Therefore $0 \leq \alpha \leq 0.4$

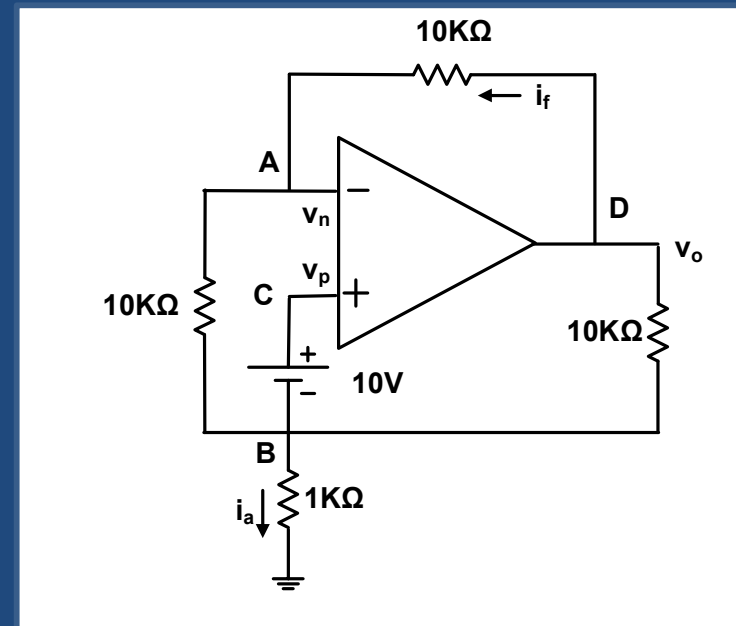


Exercise

Find the current i_a

Statement:

1. $i_p = i_n = 0$
2. $v_p = v_n$



Solution

Use node technique:

$$A: \left(\frac{1}{10K} + \frac{1}{10K}\right)v_A - \frac{1}{10K}v_B - \frac{1}{10K}v_o = 0 \quad (1)$$

$$B \& C: -\frac{1}{10K}v_A + \left(\frac{1}{1K} + \frac{1}{10K} + \frac{1}{10K}\right)v_B - \frac{1}{10K}v_o = 0 \quad (2)$$

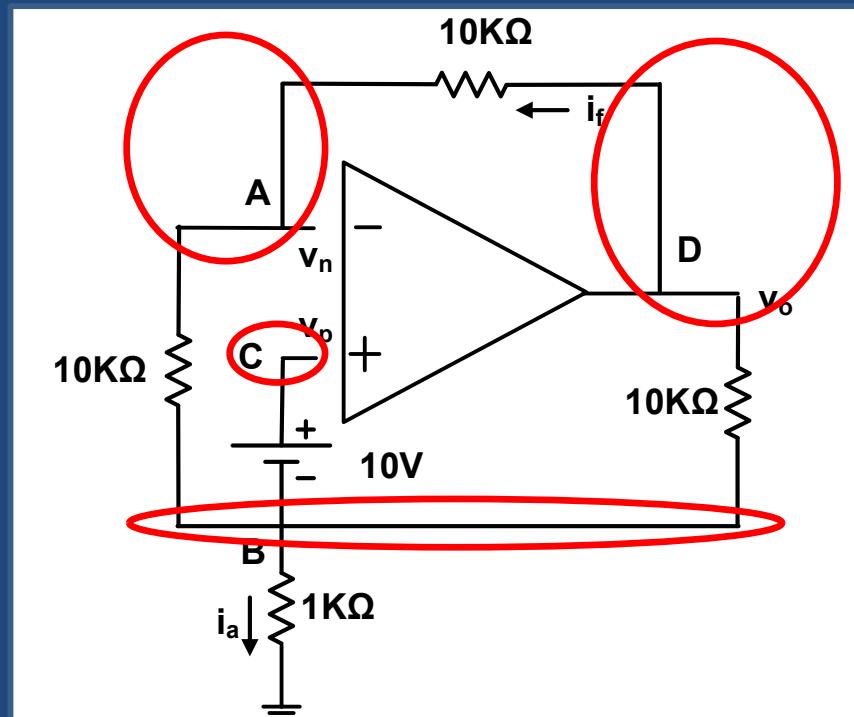
$$v_C - v_B = 10$$

$$\text{But } v_C = v_A = v_p = v_n \Rightarrow v_A - v_B = 10 \quad (3)$$

$$(1) \& (2) \Rightarrow 3v_A - 13v_B = 0 \quad (4)$$

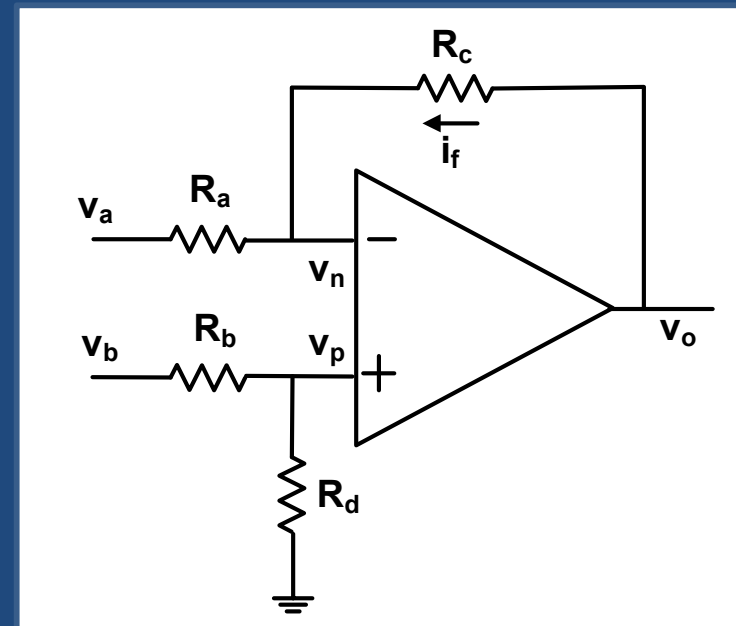
$$(3) \& (4) \Rightarrow v_B = 3V$$

$$\Rightarrow i_a = \frac{3}{1K} = \underline{\underline{3mA}}$$



Difference Amplifier

1. The goal of this circuit is to:
 - Compare 2 inputs
 - Eliminate the noise
 - Amplify the difference between 2 inputs
2. $i_p = i_n = 0$
3. $v_p = v_n$



Difference Amplifier

Use node technique:

$$A: \left(\frac{1}{R_a} + \frac{1}{R_c}\right)v_n - \frac{1}{R_a}v_a - \frac{1}{R_c}v_o = 0 \quad (1)$$

$$B: \left(\frac{1}{R_b} + \frac{1}{R_d}\right)v_p - \frac{1}{R_b}v_b = 0 \quad (2)$$

$$(1) \Rightarrow v_o = \left(\frac{R_c}{R_a} + 1\right)v_n - \frac{R_c}{R_a}v_a \quad (1')$$

$$(2) \Rightarrow v_p = \frac{R_d}{R_b + R_d} v_b = v_n \quad (2')$$

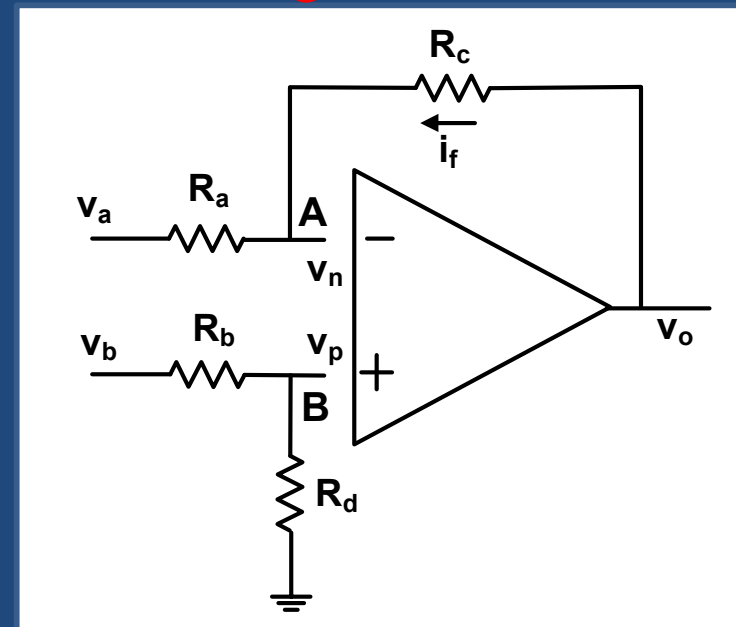
$$\Rightarrow v_o = \left(\frac{R_a + R_c}{R_a}\right) \left(\frac{R_d}{R_b + R_d}\right)v_b - \frac{R_c}{R_a}v_a \quad (3)$$

To eliminate the noise i.e., $v_o = 0$ when $v_a = v_b$

$$(3) \Rightarrow \left(\frac{R_a + R_c}{R_a}\right) \left(\frac{R_d}{R_b + R_d}\right) = \frac{R_c}{R_a}$$

Or $R_a R_d = R_b R_c$
and $v_o = \frac{R_c}{R_a} (v_b - v_a)$

Gain



Difference Amplifier: Exercise

Design this circuit with gain = 10X, $R_a = 4.7\text{K}\Omega$ and voltage source v_b sees an input resistance of 220K Ω .

$$(1) \Rightarrow 4.7\text{K} \times R_d = R_b R_c$$

$$\frac{R_c}{4.7\text{K}} = 10 \Rightarrow R_c = 47\text{K}\Omega$$

$$\text{and } (1) \Rightarrow \frac{R_d}{R_b} = \frac{R_c}{R_a} = 10$$

$$\Rightarrow R_d = 10 R_b \quad (3)$$

V_b sees an output resistance of 220K

$$\text{i.e., } R_b + R_d = 220\text{K}\Omega \quad (4)$$

$$(3) \& (4) \Rightarrow R_b + 10R_b = 220\text{K}\Omega$$

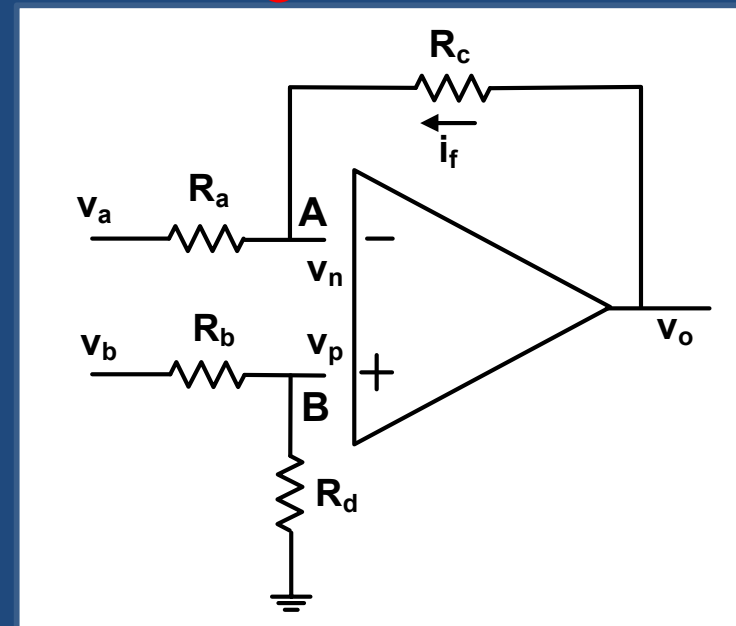
$$\Rightarrow R_b = 20\text{K}\Omega$$

$$\text{and } R_d = 200\text{K}\Omega$$

Gain = 10

$$R_a R_d = R_b R_c \quad (1)$$

$$v_o = \frac{R_c}{R_a} (v_b - v_a) \quad (2)$$



Difference amplifier: Another perspective

- Differential mode input

$$V_{dm} = v_b - v_a$$

- Common mode input

$$V_{cm} = (v_a + v_b) / 2$$

- $V_a = v_{cm} - (1/2) v_{dm}$

- $V_b = v_{cm} + (1/2) v_{dm}$

- $V_o = A_{cm} v_{cm} + A_{dm} v_{dm}$

❖ A_{cm} : common mode gain

$$A_{cm} = \frac{R_d(R_a + R_c)}{R_a(R_b + R_d)} - \frac{R_c}{R_a}$$

❖ A_{dm} : differential mode gain

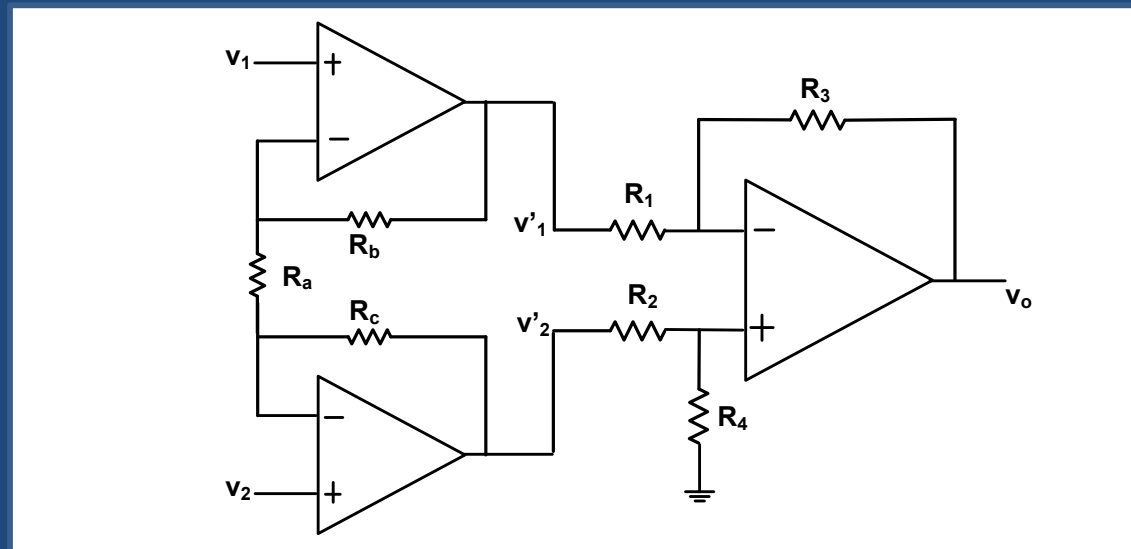
$$A_{dm} = \frac{1}{2} \left[\frac{R_d(R_a + R_c)}{R_a(R_b + R_d)} + \frac{R_c}{R_a} \right]$$

- Common mode rejection ratio:

$$CMRR = |A_{dm} / A_{cm}| \text{ (the higher the better)}$$

Instrumentation amplifier

1. Ultrahigh input impedance: 10^{15} ohm
2. High and stable linear gain: 10 to 1,000
3. High Common Mode Rejection Ratio (CMRR): >10,000 or 60-100 dB





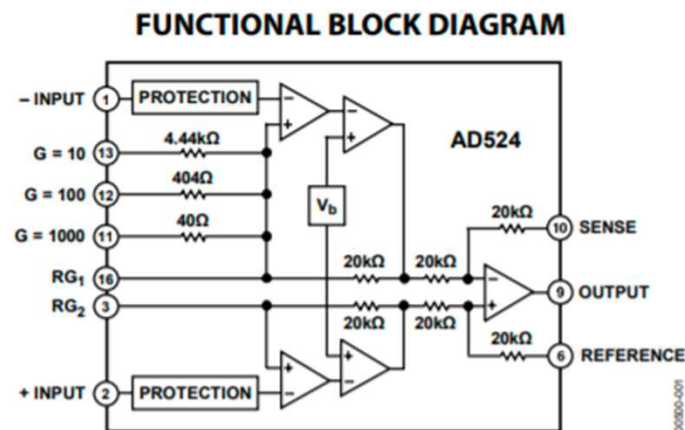
Precision Instrumentation Amplifier AD524

FEATURES

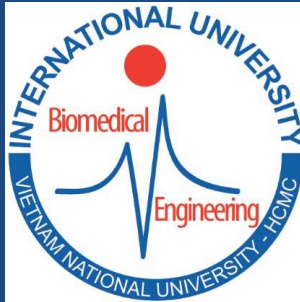
- Low noise: $0.3 \mu\text{V p-p}$ at 0.1 Hz to 10 Hz
- Low nonlinearity: 0.003% ($G = 1$)
- High CMRR: 120 dB ($G = 1000$)
- Low offset voltage: $50 \mu\text{V}$
- Low offset voltage drift: $0.5 \mu\text{V}/^\circ\text{C}$
- Gain bandwidth product: 25 MHz
- Pin programmable gains of 1, 10, 100, 1000
- Input protection, power-on/power-off
- No external components required
- Internally compensated
- MIL-STD-883B and chips available
- 16-lead ceramic DIP and SOIC packages and 20-terminal leadless chip carrier available
- Available in tape and reel in accordance with EIA-481A standard
- Standard military drawing also available

GENERAL DESCRIPTION

The AD524 is a precision monolithic instrumentation amplifier designed for data acquisition applications requiring high accuracy under worst-case operating conditions. An outstanding combination of high linearity, high common-mode rejection, low offset voltage drift, and low noise makes the AD524 suitable



higher linearity C grade are specified from -25°C to $+85^\circ\text{C}$. The S grade guarantees performance to specification over the extended temperature range -55°C to $+125^\circ\text{C}$. The AD524 is available in a 16-lead ceramic DIP, 16-lead SBDIP, 16-lead SOIC wide packages, and 20-terminal leadless chip carrier.



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